

Steam Direct Injection

Technology Overview: Steam Direct Injection

Motivation

- Waste heat (exhaust and coolant) contains ~50% of total fuel energy of gasoline ICE, which is more than the crankshaft power (at best efficiency operation)
- In part-load operation this is even more

Difficulties

- Waste Heat Regeneration cycles based on ORC or Clausius Rankine cycles are very expensive, relatively inefficient
- Additional costs and mass very high for vehicle application
- Instationary behaviour very bad, power control depending on heat up profile, typical delay time a few minutes

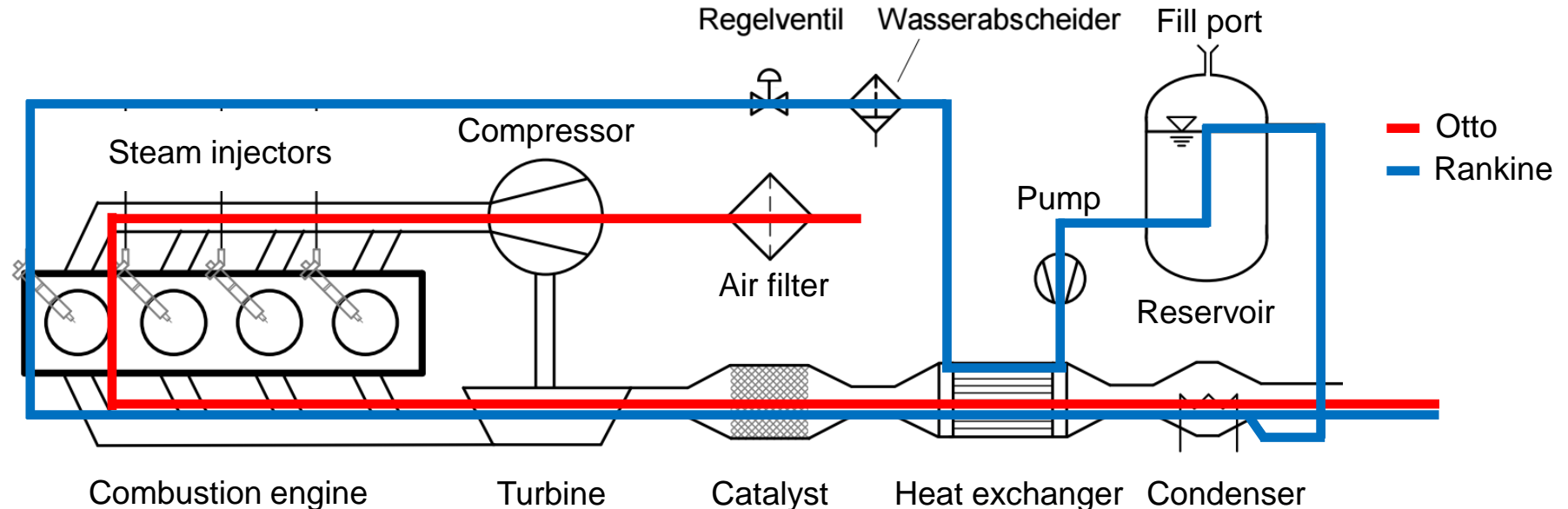
Solution

- No additional expansion unit, usage of combustion engine itself
- Dynamic behavior coupled to engine, System pressure coupled to exhaust energy

Combination of known processes in a single expansion machine is key

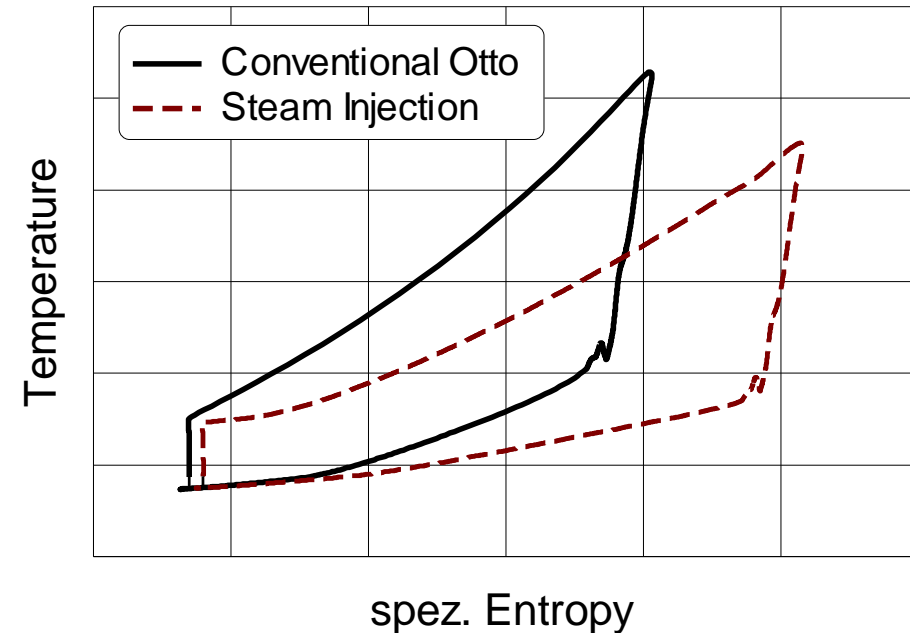
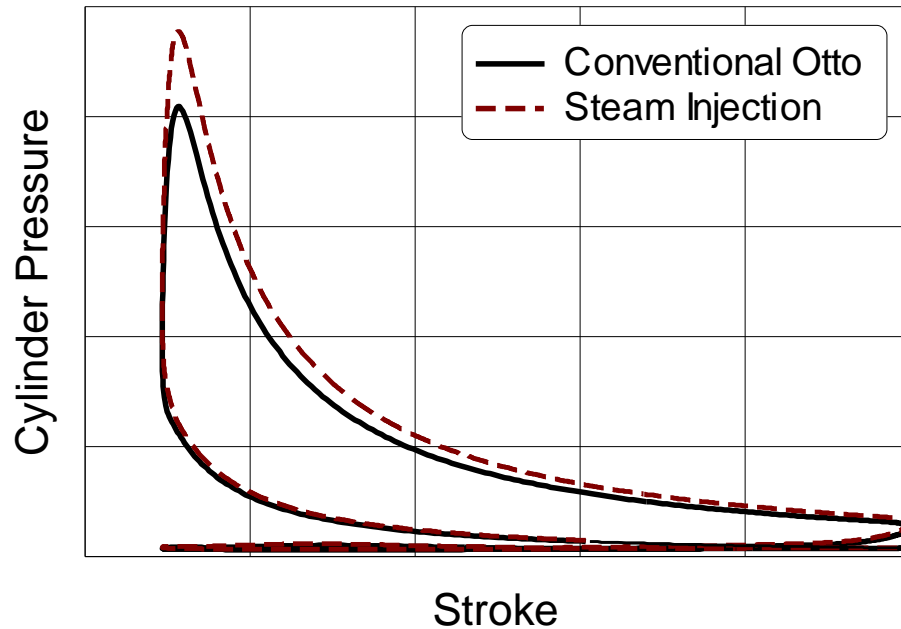
STEAM CONDITIONING AND DIRECT INJECTION

- Exhaust heat exchanger generates high pressure steam
- Steam pressure depends on waste heat energy, delayed heat up due to thermal inertia
- Steam injections depend on operating point, however it shows fast control characteristics
- Power increase and efficiency gain due to steam expansion and combustion process
- Reduction of peak temperatures and exhaust gas temperature increase component protection



P-V AND T-S DIAGRAMS

- Increased overall cylinder pressure due to increased trapped mass
- Heat supply and heat dissipation happen at lower temperature levels
- Additional mass during injection leads to higher specific entropy
- Decreased temperatures throughout the whole combustion cycle result into higher efficiency

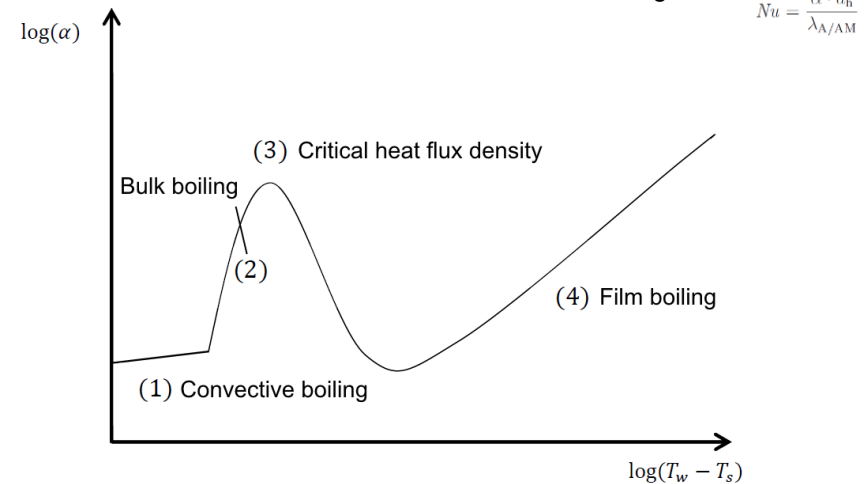
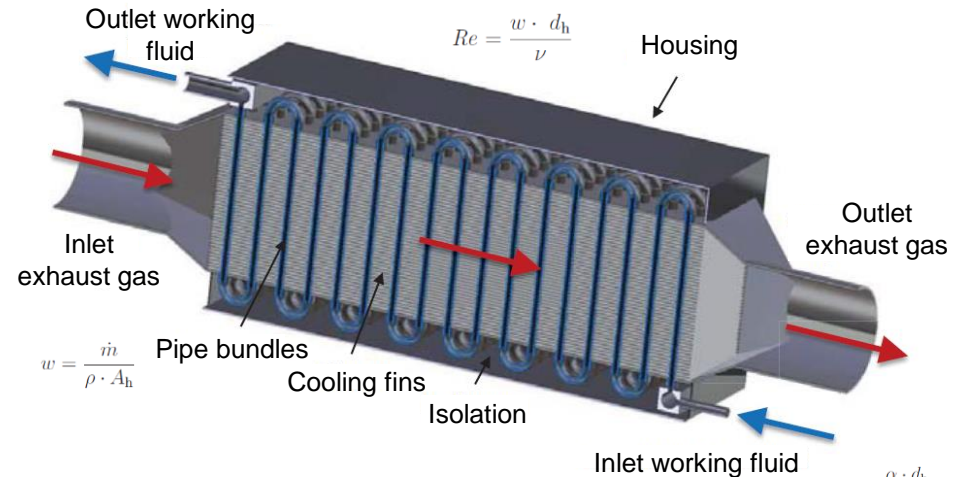


Component design

Rapid heat up vs. sufficient steam delivery rate

HEAT EXCHANGER

| Technical Design | |
|--|----------------------------|
| Max. static pressure @ Mass flux (exhaust) | 1330mbar @ 835 kg/h |
| Max. Backpressure @ Mass flux (exhaust) | 230mbar @ 835 kg/h |
| Alpha on the exhaust side | 10-120 [W/m²K] |
| Alpha on the working fluid side | 2.000-10.000 [W/m²K] |
| Pipe Diameter (Inside/Outside) | 8/12 mm |
| Nominal / Max. Pressure | 100/120 bar |
| Material | X5CrNi18-10 (V2A) |
| Length/Width/Height | 400/320/120 mm (15.4 L) |
| Interior pipe volume | |
| Max. Steam delivery rate | |



Quelle : BMW - Betrieb eines Rankine-Prozesses zur Abgaswärmenutzung im PKW

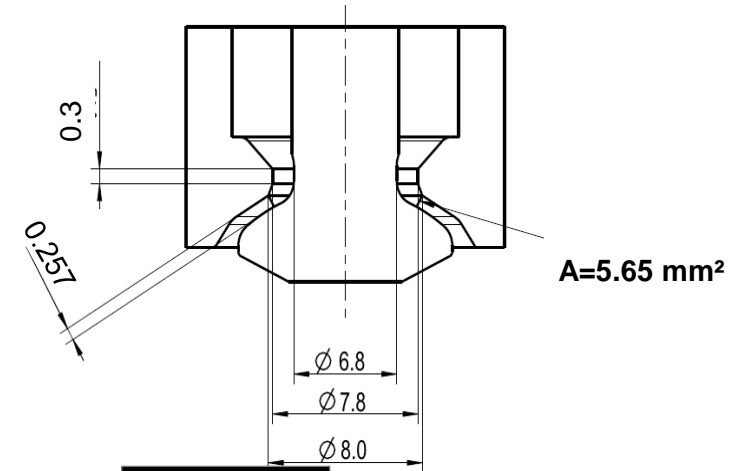
Component design of Injector for acceptable Part-load performance trade-off

INJECTOR

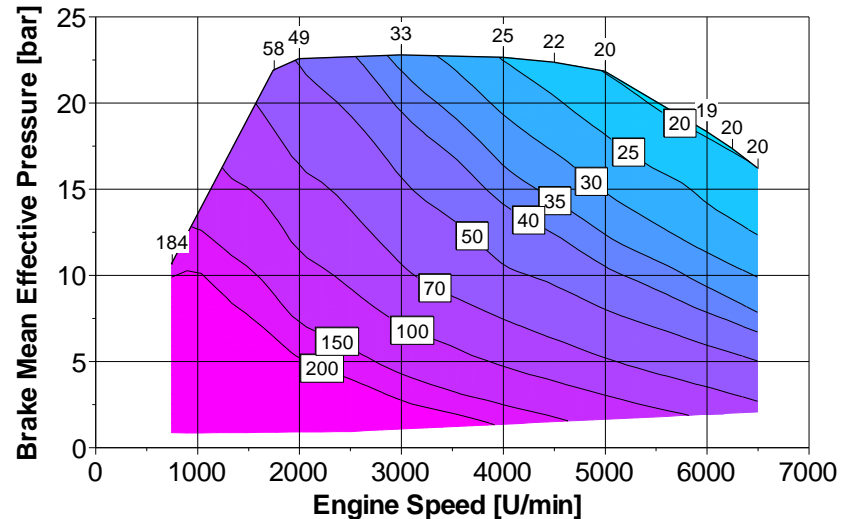
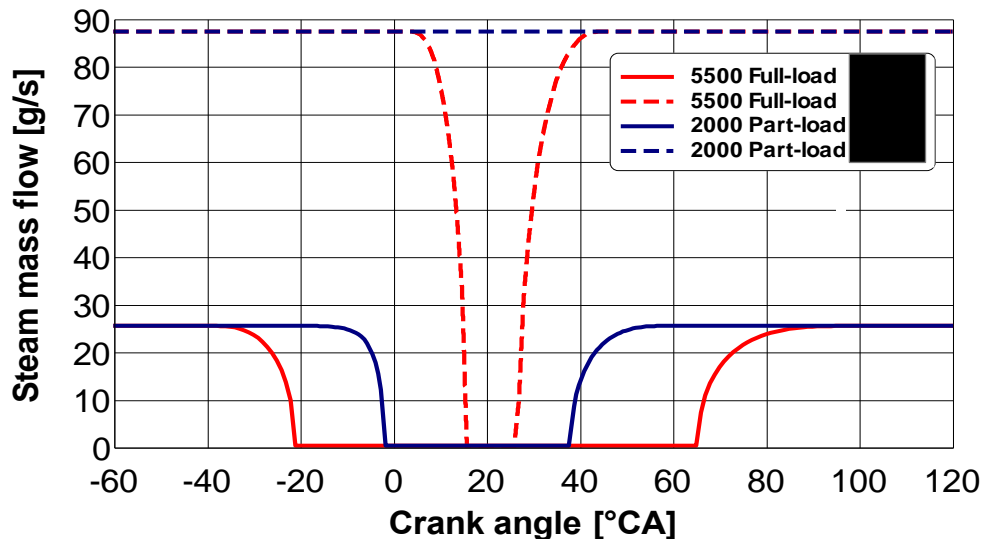
$$\dot{m}_{Inj} = A \cdot \mu \cdot \Psi(x, \kappa) \cdot \rho_{Steam} \cdot \sqrt{2 \cdot R \cdot T} \quad \text{with } x = \frac{p_{Cyl}}{p_{Inj}}$$

46 times more dense than air at 20°C

$$\Psi = \begin{cases} \left(\frac{2}{\kappa+1}\right)^{\frac{1}{\kappa-1}} \cdot \sqrt{\frac{\kappa}{\kappa+1}} & x \leq \left(\frac{2}{\kappa+1}\right)^{\frac{\kappa}{\kappa-1}} \\ \sqrt{\frac{\kappa}{\kappa-1} \cdot \left[x^{\frac{2}{\kappa}} - x^{\frac{\kappa+1}{\kappa}}\right]} & \left(\frac{2}{\kappa+1}\right)^{\frac{\kappa}{\kappa-1}} < x < 1 \end{cases}$$



Max. rel. steam mass at $\Delta\alpha_{max}$ at operation with [redacted]

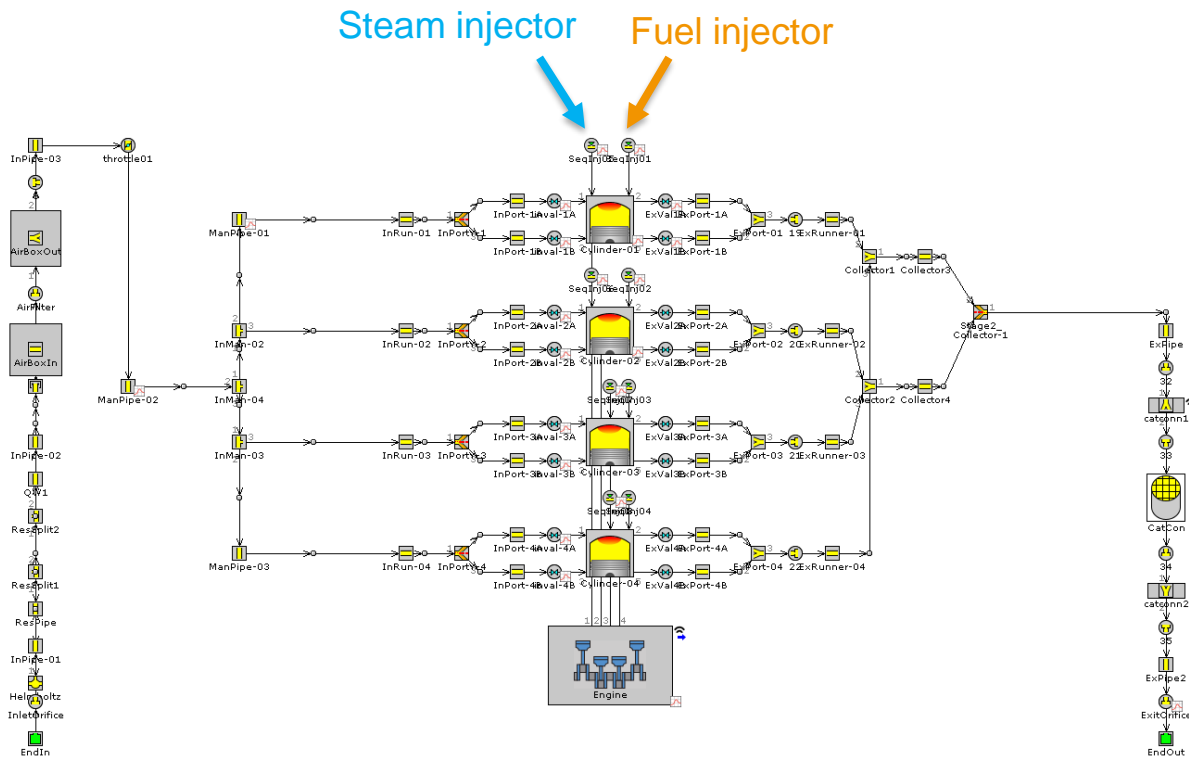


Simulation model

Crank angle resolved model illustrates the steady behavior



GT-POWER MODEL - STEADY STATE



Steam injector Fuel injector



Background

- No test engine with direct steam injectors available
- 1-D Simulation tools used to simulate the behavior
- The baseline model is tuned with readings from the engine test bench
- The steady state behavior lies in focus
- Steam injectors were implemented as described previously
- Steam injection is overlaid onto baseline burn rate to avoid side effects

Engine displacement : 2.2 L

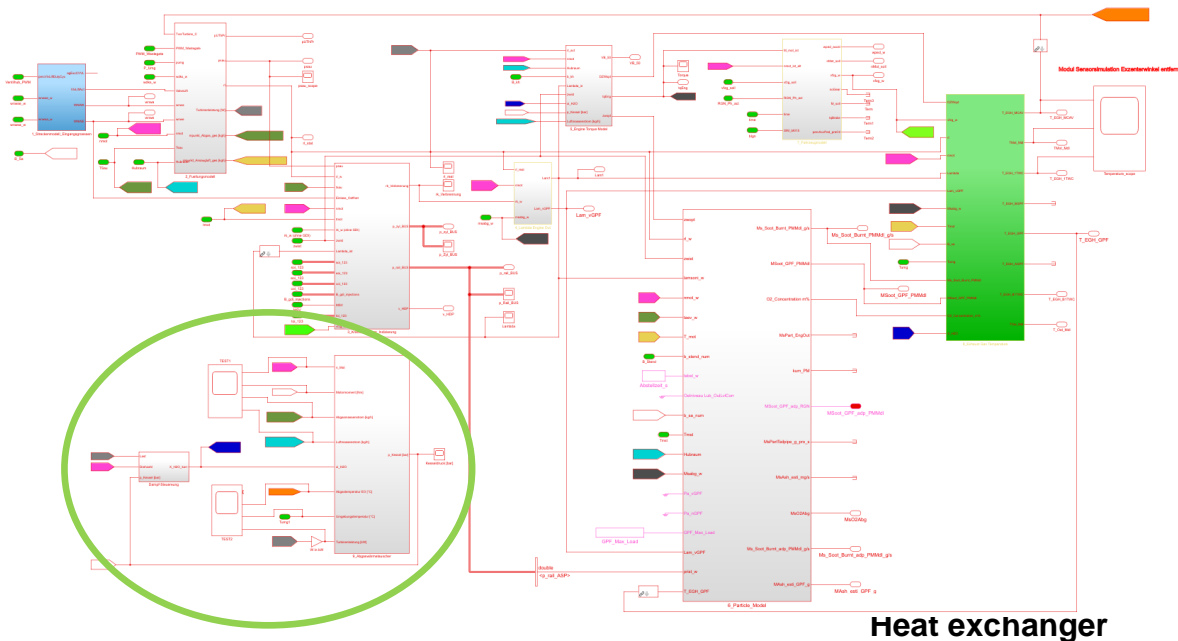
Vehicle gross weight : 2830 kg

Simulation model

Time resolved model illustrates dynamic behavior and cross-interference



SIMULINK MODEL – DYNAMIC



Background

- Component heat up is simulated
- The whole exhaust gas system needs to be simulated to determine the exhaust energy at the heat exchanger
- Time constants have been derived from real world measurements
- Steam pressure can be monitored
- A pressure based steam control strategy is implemented
- The model allows to simulate prebuild driving cycles such as WLTP and RDE

Simulation results

Taking full advantage of early steam injections is key to high efficiency



PART LOAD PERFORMANCE - 2000RPM 11BAR – 100BAR INJECTION

Steam injection

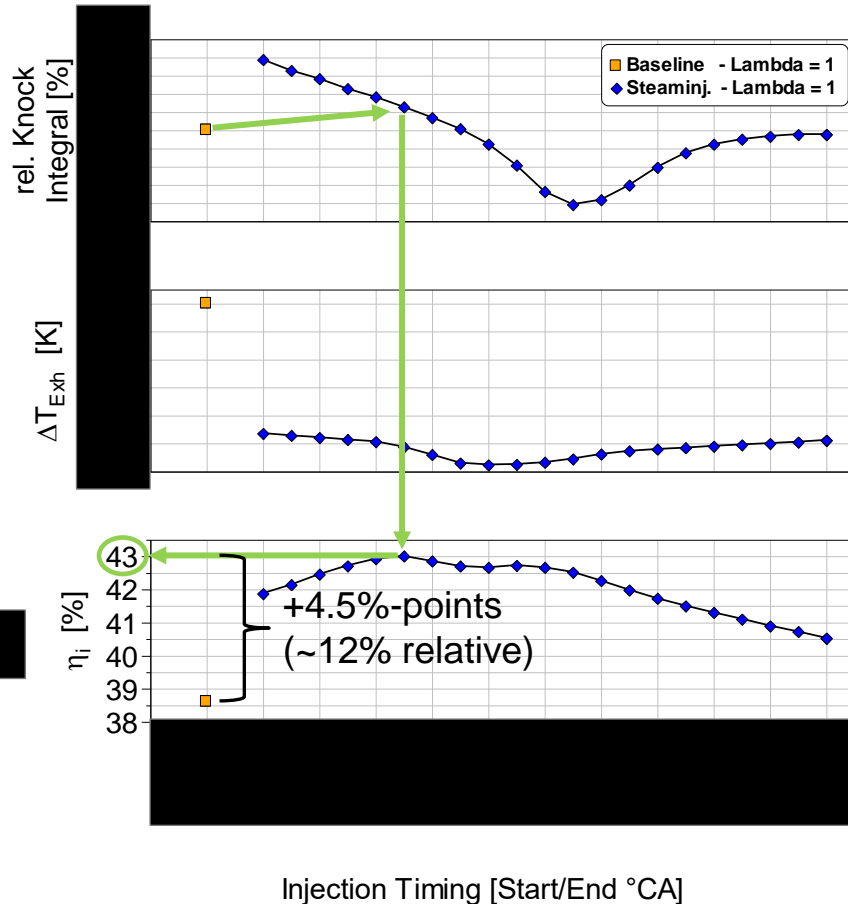
Simulation Results

Load point: 2000 rpm / 11 bar

Relative steam mass relating to intake air = 20%

Engine

| | |
|---------------------|------------|
| Bore: | 89 mm |
| Stroke: | 88.3 mm |
| Cylinder.: | 4 |
| Intake Valve Lift: | 8.8 mm |
| Exhaust Valve Lift: | 9.0 mm |
| Vse_in: | 81° |
| Vse_out: | 90° |
| MBF50%: | 5.7° |
| MBF10/90: | 17° |
| Amb.Temp.: | 20 °C |
| Steam mass: | [REDACTED] |
| Puls duration: | [REDACTED] |



GT-Power Results

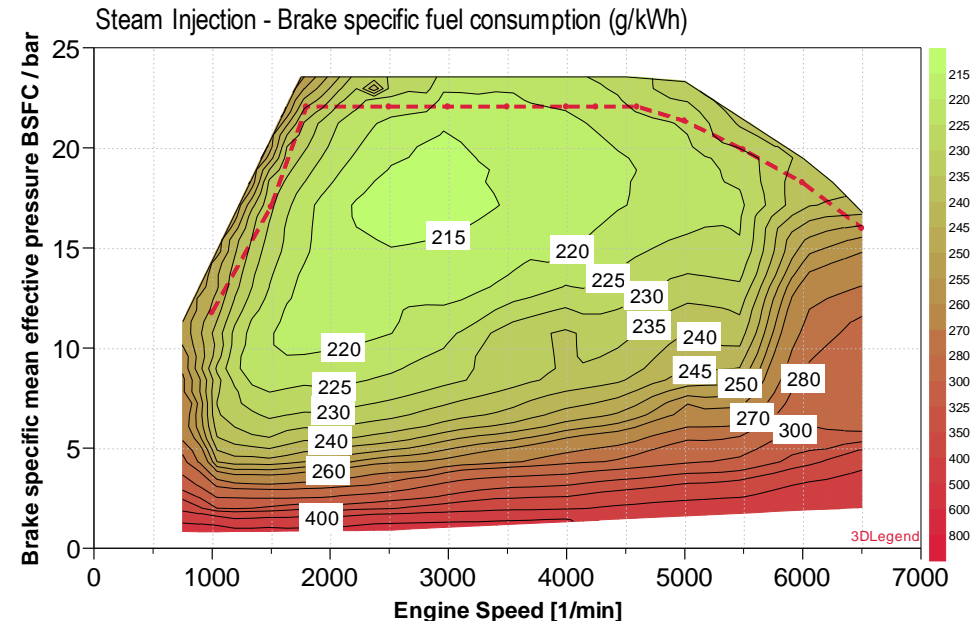
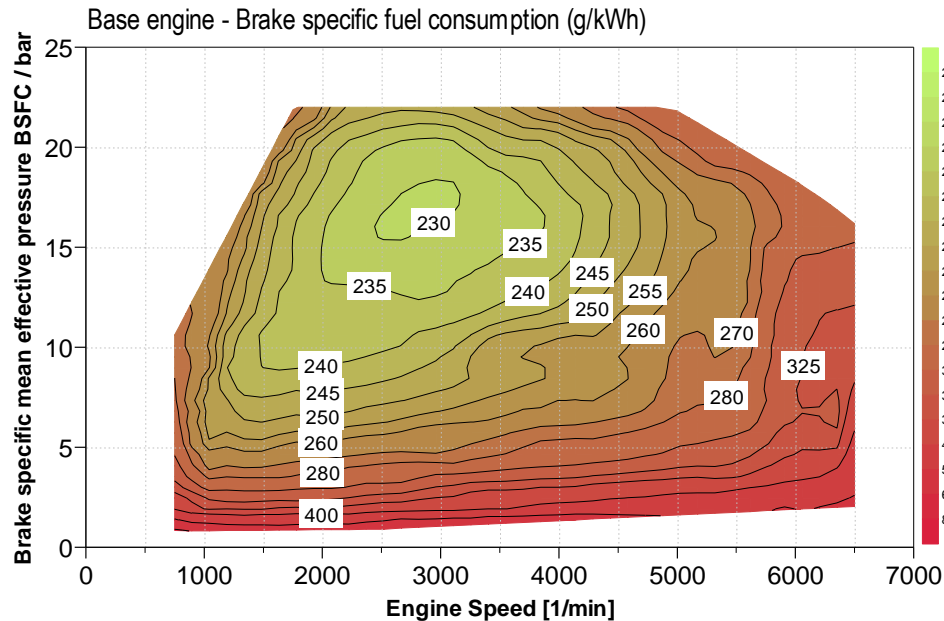
- Low rotational speed allows for short injection timing [REDACTED]
- Load point stability enables pre p_{max} injections leading to higher efficiency
- Combustion peak temperature can be lowered significantly by [REDACTED]
- Decreased exhaust temperature beneficial for component protection
- Since the baseline point is not knock limited, the efficiency gain can be pushed even further by allowing operation at a higher rel. knock level than baseline

Simulation results

Relevant engine operation points

STEAM INJECTION ENGINE MAP - OVERVIEW

- Steam injections enable $\lambda = 1$ operation on the entire engine map
- Higher efficiency leads to lower specific consumption (minimal 215 g/kWh)
- Furthermore the area of up to 230 g/kWh is expanded
- The peak torque can be achieved at lower engine speed

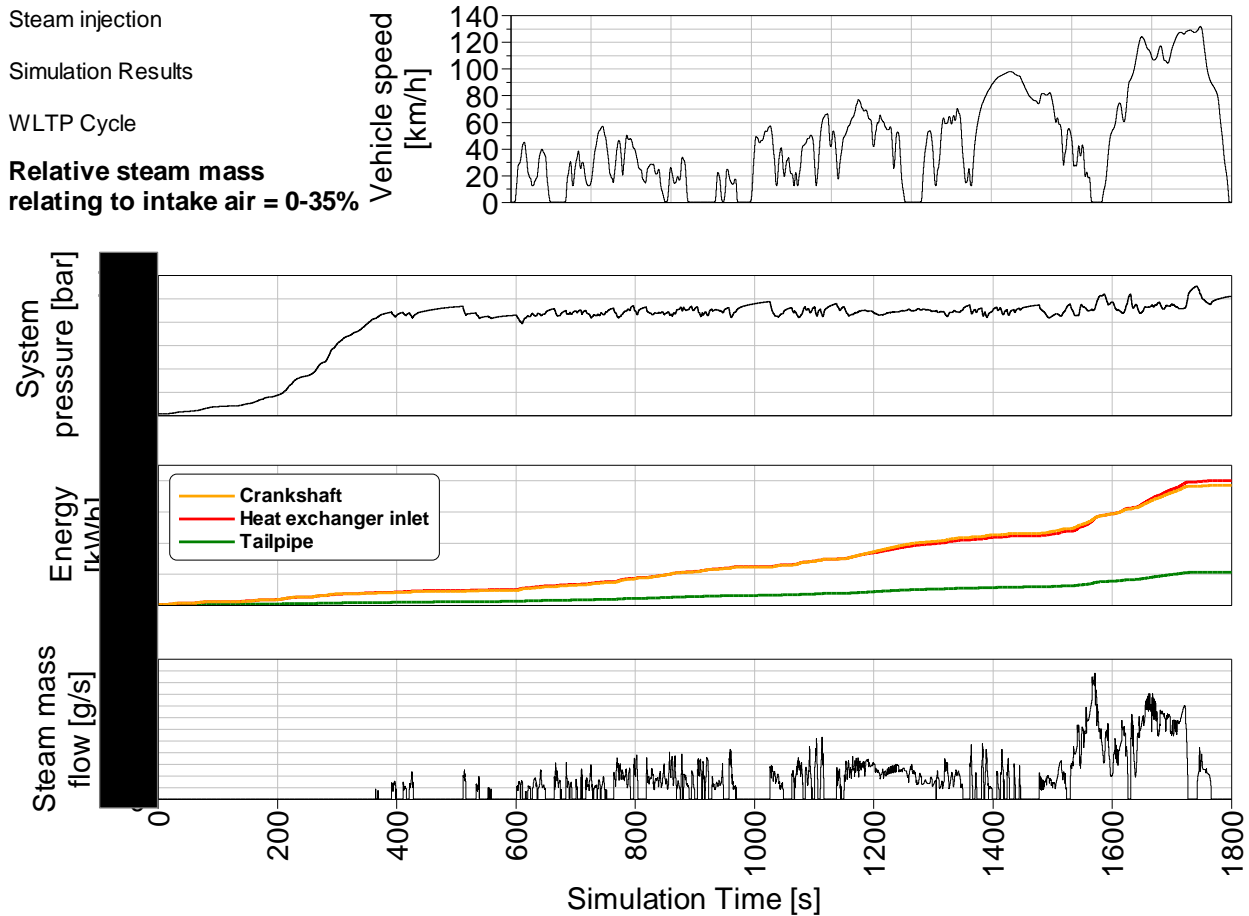


Simulation results

WLTP takes full advantage of fast heat up and torque boost



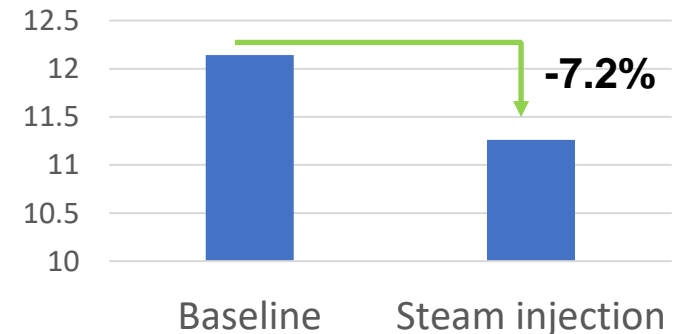
CYCLE SIMULATION WLTP



Cycle Simulation Results

- The heat exchanger is able to extract a significant amount of energy from the exhaust gas
- After short heat up period (365s) the system is fully operational
- 25.8L/100km water consump.

Fuel consumption [L/100km]



Simulation results

Overall benefit of in-cycle fuel consumption comes at a cost



COST ESTIMATE

| Component | Estimate |
|----------------------------------|-----------------|
| Heat Exchanger | 100-200 € |
| Injector | 4x50 € |
| High Pressure Pump | 25 € |
| Reservoirs e.g.(SCR Tank) | 10-30 € |
| Piping and Isolation Material | 15-40 € |
| Recuperator | 50-120 € |
| Water separator + Valves | 5-15 € |
| | |
| Sum | 405-630€ |

| Opportunities | Challenges |
|---|--|
| <ul style="list-style-type: none"> ■ Up to 21 g/km CO₂ reduction in WLTP ■ Enables $\lambda = 1$ operation at all load points ■ Overall torque boost increases peak power output ■ Synergy effects with liquid water injection / use of common components | <ul style="list-style-type: none"> ■ Condensation along the piping must be prevented ■ Water freezing must be prevented ■ High water consumption → water recuperation system necessary ■ Validation of real combustion process necessary |

Steam Direct Injection

Key facts

Key facts Steam direct injection

- Steam generation by Exhaust heat exchanger up to 5-50bar
- Steam Power available on demand
- No additional expansion device necessary, steam injection into main engine
- Part-efficiency of bottom cycle up to 30%
- Maximum Power gain (for limited time) ~10kW
- Additional positive influence to base engine
 - Soot reduction by agglomeration and peak combustion temperature reduction
 - Component protection included due to lower exhaust gas temperatures – all Lambda 1

Key facts Turbo Steamer

- Steam generation by Exhaust heat exchanger up to 5-50bar
- Continuous steam power generation, independent from usage
→ needs to be buffered
- Expansion device is turbine or cell expander, efficiency strongly dependent on OP point
- Cycle efficiency including pinch-effect 10..15%
- Electrical power generation of max. 2kW